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26      12      36      6      26  
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 26      12      36      5      24  
 fl ' Ț fl''\* Ț ( 8 ) ( 2 ) ( 0 ) fl ' Ț  
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4	152	594	< *
4	108	446	< %
6	30	180	< *
4	72	288	< %
6	8	48	< %

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3	26	78	$\frac{fl}{fl}$	$\frac{t}{t}$	0.76	<*,
2	37	74	$\frac{fl}{fl}$	$\frac{t}{t}$	0.82	<*,
3	22	66	$\frac{fl}{fl}$	$\frac{t}{t}$	0.71	<*,
2	118	236	$\frac{fl}{fl}$	$\frac{t}{t}$	1.00	<*



2	19	38	0.81	<*
3	8	24	0.87	<*
4	13	52	1.28	<*
4	19	76	0.46	< -
4	14	56	0.58	< -
4	33	132	0.51	< +
4	17	68	0.60	< -
4	21	84	0.98	< -
4	14	56	0.87	< +
4	36	144	1.83	< ,
4	16	64	1.37	< +
4	40	160	1.28	< +

2	21				0.87	
2	20	40			1.10	<-%%
2	100	200			0.92	<%%
3	50	150			0.96	<%(
4	10	40			0.32	<%(
2	53	106			0.82	<' (
3	32	96			0.96	<' (
2	38	76			1.48	<-%%
3	18	54			0.90	<-%%
2	24	48			1.45	<-%\$
3	12	36			0.46	<-%\$
2	25	50			1.36	<-%\$
3	11	33			0.78	<-%\$
2	54	108			0.76	<-%\$
3	23	69			0.41	<-%\$
2	53	106	fl	ε	1.20	<+%
3	24	72	fl	ε	1.23	<+%
2			fl	ε		<-%*
3			fl	ε		<-%*
2	46	92	fl	ε	0.69	<-%
3	20	60			0.86	<-%
2	18	36			1.19	<-%\$
3	7	21			0.28	<-%\$
2	18	36			1.41	<-%
3	8	24			0.62	<-%
2	38	76	fl	ε	1.07	<-%
3	16	48	fl	ε	0.56	<-%
2	32	64			1.18	<-%
3	14	42			0.32	<-%
2	20	40	fl	ε	1.32	<-%
3	10	30			0.40	<-%
2						<-%
3						<-%
2	27	54			1.40	<-%
3	12	36			0.58	<-%
2	25	50			1.14	<-%
3	9	27			0.66	<-%
2	25	50			1.14	<-%
3	9	27			0.33	<-%
2	28	56			1.94	<-%
3	12	36			1.08	<-%
2	24	48			1.74	<-%
3	8	24			1.62	<-%
2	29	58			1.03	<-%
3	12	36			0.52	<-%
2	100	200	fl	ε	0.84	<-%&
3	44	132	fl	ε	0.64	<-%&
3	6	12			0.58	<-%

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